

NOWCASTING THE VARIATION OF WIND SPEED WITH HEIGHT USING GUST FACTOR MEASUREMENT

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Abstract

In the atmospheric surface boundary layer from the ground level up to a few hundred feet, the wind speed normally increases with height under near-neutral conditions. Knowledge of the vertical variation of the wind speed is important to operational meteorologists so that they can provide reasonable estimates to emergency managers and structural engineers. For example, during hurricane conditions in New Orleans, Louisiana, what would be the expected wind gust on the elevated bridges crossing the Mississippi River? What would be the expected wind loading on a high-rise building which might be used as a vertical evacuation shelter? This increase in wind speed is often estimated operationally using the power-law wind profile. However, its exponent needs to be determined objectively. This note provides a solution through the utilization of gust factor measurements. It is shown that the formula $G = 1 + 2.88P$ is verified under the conditions of one tropical storm and ten hurricanes for a total of 148 samples as measured from various airports, where G is the gust factor (i.e., the ratio of wind gust to the mean wind speed) and P is the exponent of the power-law profile.

1. Introduction

From time to time an operational meteorologist may be called upon to assist in the determination of the variation of wind speed with height at an elevation other than 10 m, the typical Automated Surface Observing System (ASOS) height. Nowcasting this vertical distribution of the wind speed is often needed, particularly during storm conditions or for emergency preparedness (such as the event of an industrial fire) when routine weather measurements are available from airports located in the general region of the accident. This note intends to provide a rapid estimation for this practical application using the gust factor measurement for input.

2. Method and Justification

In the atmospheric surface boundary layer which extends from the ground up to a few hundred feet, the wind speed generally increases with height.

Operationally, this power-law wind profile is often used (e.g., Panofsky and Dutton 1984)

$$v_2 = v_1 \left(\frac{z_2}{z_1} \right)^P \quad (1)$$

where v_1 is the reference (or known) wind speed (e.g., from ASOS) at the known height of z_1 (e.g., 10 m), v_2 is the wind speed needed at the height of z_2 , and P is the exponent of this power-law profile.

According to Simpson and Riehl (1981, p. 202), for open country near the coastline, $P = 1/7 = 0.14$. Since airports are normally located in the open country, we use the wind measurements from airports for this study. Under near-neutral conditions, P varies with the roughness length, z_0 , which is a function of surface irregularities (i.e., average spacing and height of surface features (Simpson and Riehl 1981, p. 201)). According to Justus (1985, p. 922), $P = 0.13$ when the roughness $z_0 = 0.01$ m and $P = 0.19$ when $z_0 = 0.1$ m. Because these variations are not linear, we use the power-curve fit as follows: let

$$P_1 = a z_{01}^b \quad (2a)$$

where $P_1 = 0.13$ and $z_{01} = 0.01$ m and

$$P_2 = a z_{02}^b \quad (2b)$$

where $P_2 = 0.19$ and $z_{02} = 0.1$ m. Solving Eqs. (2a) and (2b) simultaneously using the known boundary conditions, we get

$$P = 0.278 z_0^{0.165} \quad (2c)$$

for the z_0 range between 0.01 and 0.1 m. According to Panofsky and Dutton (1984, p. 123), $z_0 = 0.025$ m for airports (runway area). Substituting this z_0 into Eq. (2c), we have

$$P = 0.15 \quad (3)$$

This supports $P = 0.14$ as recommended in Simpson and Riehl (1981) as reasonable.

Based on the formula for estimating wind maxima as suggested in Panofsky and Dutton (1984, p. 376), a rela-

Table 1. Measured Gust Factors During ten Hurricanes and one Tropical Storm at Various Airports (Data sources: Pasch et al. (2001), Lawrence et al. (2001), and Franklin et al. (2001))

Hurricane	Station	G	Hurricane	Station	G	Hurricane	Station	G
Bonnie	St. Thomas AP U.S. V.I.	1.43	Mitch	Homestead AFB	1.75	Irene	Key West Intl. AP	1.24
1998	Charleston Intl. AP	1.32	continued	Tamiami AP	1.65	1999	Tamiami AP	1.33
	Florence AP	1.29		Miami Intl. AP	1.95		Homestead AFB	1.76
	Oceana NAS	1.42		Opalocka AP	1.36		Miami Intl. AP	1.49
	Langley AFB	1.26		Fort Lauderdale AP	1.24		Pompano Beach AP	1.25
	Norfolk AP	1.40		Fort Lauderdale Ex. AP	1.36		Fort Lauderdale Ex. AP	1.25
	Norfolk NAS	1.33		Pampano Beach AP	1.39		Opalocka AP	1.26
Earl	Moisant Intl. AP	1.24		Naples AP	1.50		West Palm Beach AP	1.43
1998	New Orleans Lakefront AP	1.10		Vero Beach AP	1.68		North Perry AP	1.35
	Pascagoula/Trent Lott AP	1.38		Patrick AFB	1.37		Orlando Intl. AP	1.27
	Mobile Regional AP	1.22		Fort Pierce AP	1.45		Melbourne AP	1.45
	Mobile Brookley Field	1.29		Orlando Intl. AP	1.26		Vero Beach AP	1.59
	Dothan AP	1.41		Tampa AP	1.64	Lenny	V.C. Bird Intl. AP	1.43
	Pensacola Regional AP	1.53		MacDill AFB	1.83	1999	Hamilton AP St. Croix	1.33
	Pensacola NAS	1.34		Sarasota AP	1.67		Cyril King AP St. Thomas	1.33
	Hurlburt Field AFB	1.42		Fort Myers Regional AP	1.22		Luis Martin AP	1.17
	Whiting Field (Milton)	1.61	Bret	Brownsville AP	1.62	Opal*	NEW	1.40
	Panama City AP	1.28	1999	Cameron City AP	1.28	1995	MEI	1.50
	Marianna Municipal AP	1.31		Harlington AP	1.26		MOB	1.53
	Tallahassee Regional AP	1.38		McAllen AP	1.32		MXF	1.90
	Perry-Foley AP	1.33		Kingsville NAS	1.26		MGM	1.33
	Cross City AP	1.37	Dennis	Cherry Pt. Marine Corps.	1.29		AUB	1.92
	Tampa AP	1.22	1999	Wilmington AP	1.26		BHM	1.57
	MacDill AFB	1.42		Norfolk AP	1.24		ANB	1.38
	Sarasota AP	1.28		Langley AFB	1.47		HSV	1.32
	Regional SW AP	1.26	Floyd	Fort Lauderdale Ex. AP	1.43		NPA	1.26
Georges	Hamilton AP, St. Croix	1.23	1999	Fort Lauderdale Intl. AP	1.44		HRT	1.68
1998	Cyril E. King AP, St. Thomas	1.23		Melbourne AP	1.31		PAM	1.36
	Luis Martin AP P.R.	1.17		Patrick AFB	1.16		AQQ	1.86
	Roosevelt Roads NAS	1.22		Tamiami AP	1.48		TLH	1.64
	Patrick AFB	1.53		Savannah AP	1.31		BKV	1.40
	Miami Intl. AP	1.33		Charleston Intl. AP	1.32		TPA	1.82
	Tamiami AP	1.73		Florence AP	1.50		PIE	1.54
	Tampa AP	1.50		Seymour Johnson AFB	1.33		ATL	1.57
	MacDill AFB	1.85		Wilmington AP	1.39	T.S. Frances	Acadiana Regional AP	1.30
	Sarasota AP	1.24		Langley AFB	1.38	1998	Jefferson Parish AP	1.30
	Regional SW AP	1.54		Norfolk AP	1.48		Lake Charles AP	1.25
	Tallahassee AP	1.21		Norfolk NAS	1.26		Lafayette Regional AP	1.30
	Panama City AP	1.54		Patuxent NAS	1.20		Galveston AP	1.27
	Milton/Whiting Field	1.32		Newark Intl. AP	1.21		Houston Intl. AP	1.29
	Hurlburt AFB	1.57		Teterboro AP	1.58		Houston/Hobby AP	1.25
	Eglin AFB	1.88		Farmingdale AP	1.61		Palacios AP	1.59
	Pensacola AP	1.32		Islip/MacArthur AP	1.37		Corpus Christi NAS	1.31
	Pensacola NAS	1.53		JFK Intl. AP	1.37			
	Mobile Regional AP	1.25		LaGuardia AP	1.37		GRAND MEAN	1.42
	Mobile Brookley Field	1.15		Montgomery AP	1.52		Standard Deviation	0.18
	Gulfport AP	1.50		Montauk Point AB	1.68		Coefficient of Variation	13%
	Pascagoula/Trent Lott AP	1.31		Westhampton AP	1.54			
	Moisant Intl. AP	1.31		White Plains AP	1.68			
	New Orleans Lakefront AP	1.23		Bridgeport AP	1.34			
Mitch	Key West AP	1.37		Danbury AP	1.40			
1998	Boca Chica NAS	1.52		Meridan Markham AP	1.70			
	Marathon AP	1.67						

*from Hsu (2001)

tionship between the gust factor and P has been proposed by Hsu (2001, Eq. 2) that, under near-neutral conditions,

$$G = 1 + 2.88 P \quad (4)$$

Therefore, using Eq. (1) the wind speed at any height in the atmospheric surface boundary layer, which is typically between the ground and 100 m, can be estimated if P can be determined objectively. With the gust factor measurements, this is accomplished by applying Eq. (4).

The purpose of this note is to further verify Eq. (4) so that Eq. (1) may be correctly applied for operational use. First, we need to define what is meant by "near-neutral stability". According to the Pasquill stability classification (see, e.g., Panofsky and Dutton 1984, p. 242), the neutral class D should be assumed for overcast conditions during day or night or whenever the wind speed is higher than 6 m s^{-1} except under strong incoming solar radiation (i.e., when the solar altitude is greater than 60° with clear skies (see Hsu 1988, p. 193)). On the other hand, since the minimum gust speed reported by ASOS is 7 m s^{-1} (or 14 kt), and since the minimum G is 1.0, the hourly mean wind speed of 7 m s^{-1} exceeds the required 6 m s^{-1} . Thus one may safely assume that the gust factor measurements for ASOS can be applied under near-neutral stability conditions. Note that neutral stability exists when mechanical turbulence dominates the thermal stratification or buoyancy effect.

In order to verify Eq. (4), a large sample representing a similar environment (such as from airports) is required. In the data sets compiled by Pasch et al. (2001), Lawrence et al. (2001), and Franklin et al. (2001) there were 10 hurricanes and one tropical storm yielding a total of 148 samples for use in this analysis. These data are listed in Table 1. Analyses of these data indicate that the grand mean of the gust factor for these 148 samples is 1.42 and the standard deviation is 0.18. In order to estimate the dispersion of this data set, the coefficient of variation is employed, which is the ratio of standard deviation to mean so that $0.18 / 1.42 = 12.7\%$. If we accept this 13% value as reasonable, then $G = 1.42$ is a useful magnitude to proceed further.

3. Conclusion

Now, substituting $G = 1.42$ into Eq. (4), we get $P = 0.15$. Since this value is the same as Eq. (3), we conclude that Eq. (4) can be used to get P objectively from G and then this P can confidently be employed in Eq. (1) for operational applications such as nowcasting. Since Eq. (4) is verified, it may be applied to other environments on land if G is available. Note, that if the mean wind speed is less than 6 m s^{-1} (or 12 kt), P is a function of not only Z_0 but also stability. In this regard, the method to estimate P provided in Justus (1985) should be consulted.

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